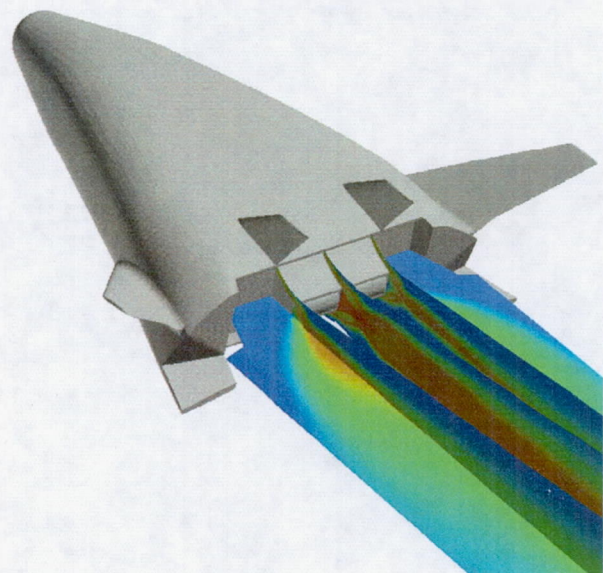


Analysis of X-33 Linear Aerospike Plume Induced Base-Heating Environment During Power-Pack Out



Ten-See Wang

Robert Williams and Alan Droege

Mark D'agnostino and Young-Ching Lee

Stan Douglas

NASA – Marshall Space Flight Center

April 4-5, 2001



Acknowledgment



- John Suter of X-33 Program Office

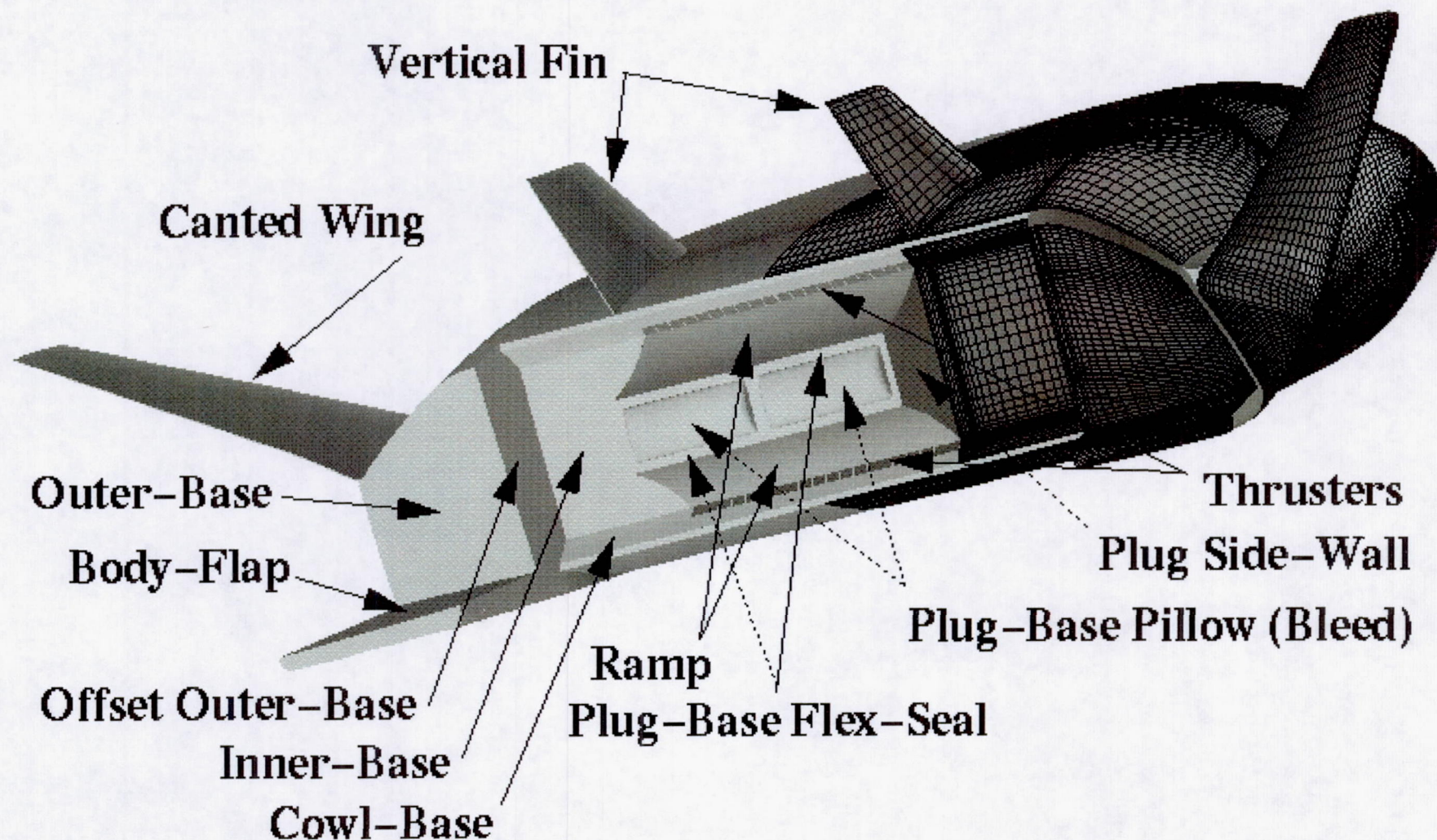


CFD Analysis of X33 Flex Seal Environments During PPO

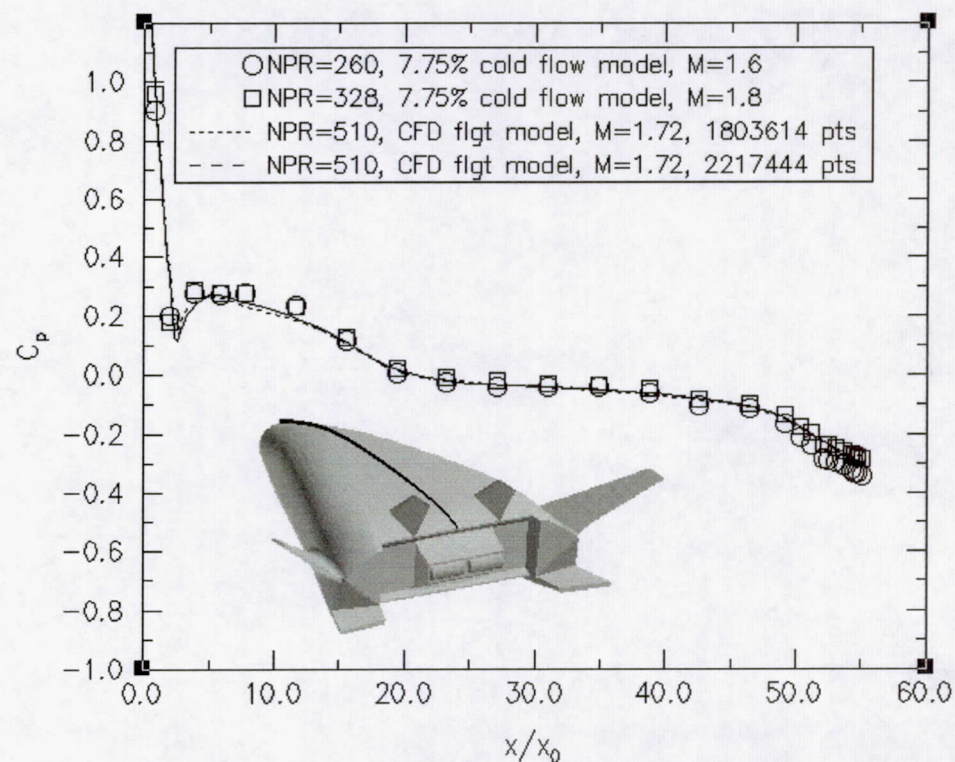
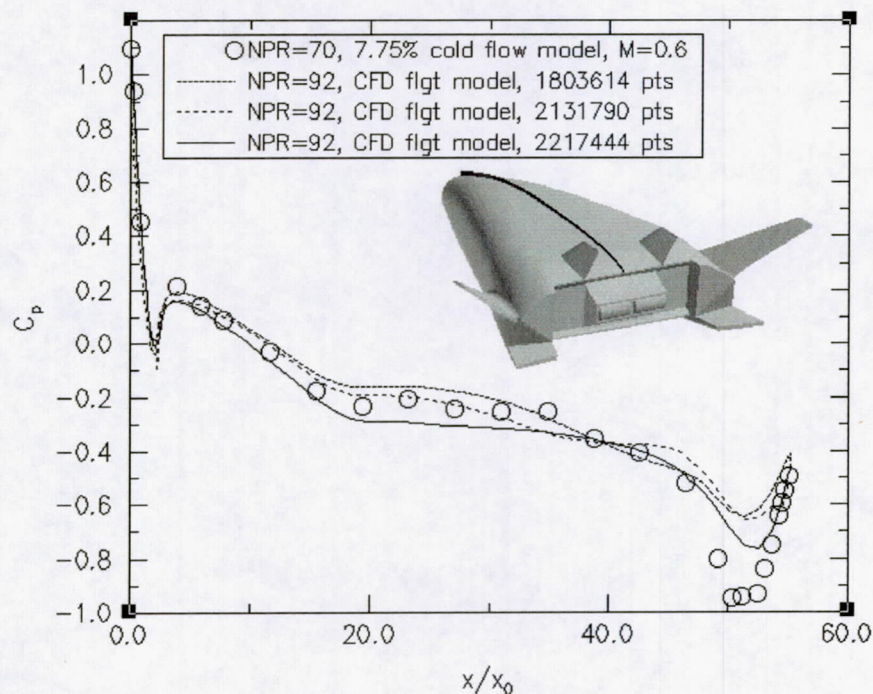


- Objective
 - Predict dual-engine base-heating at 57% PL at sea level
 - Predict dual-engine base-heating during PPO at 3 ascent abort trajectories
- Approach
 - 3D turbulent chemically reacting computational fluid dynamic and heat transfer analysis (FDNS, GASRAD and GRASP)
 - Full-vehicle and slip stream effects with dual-engine, 40-thruster, and base-pillow bleeds
 - Benchmarks
 - 7.75% scaled model cold flow test
 - 2.25% scaled model hot flow test
 - Installed full-scale engine hot-fire test

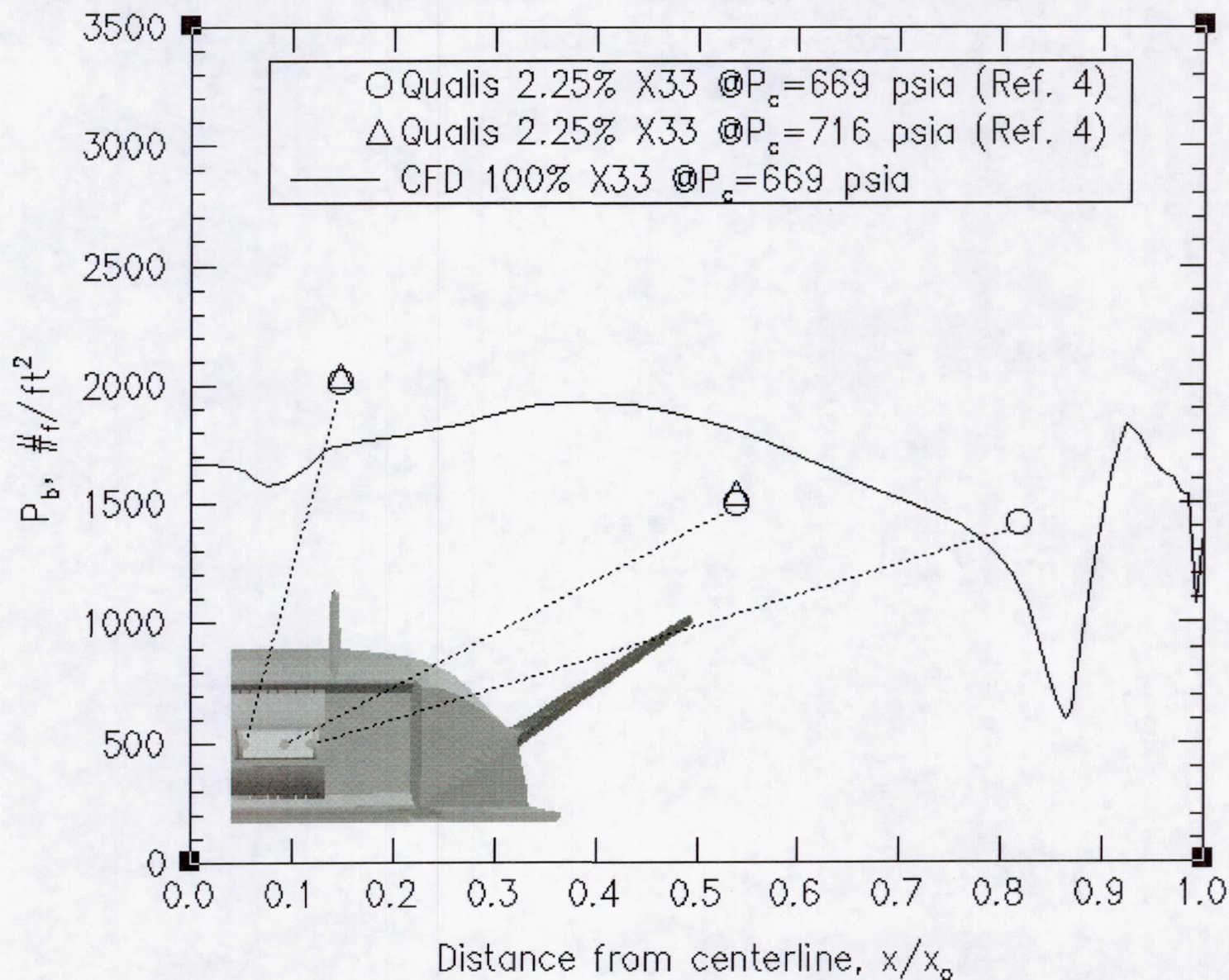
Layout of an X-33 Full-vehicle Surface Computational Grid with Surface Definitions



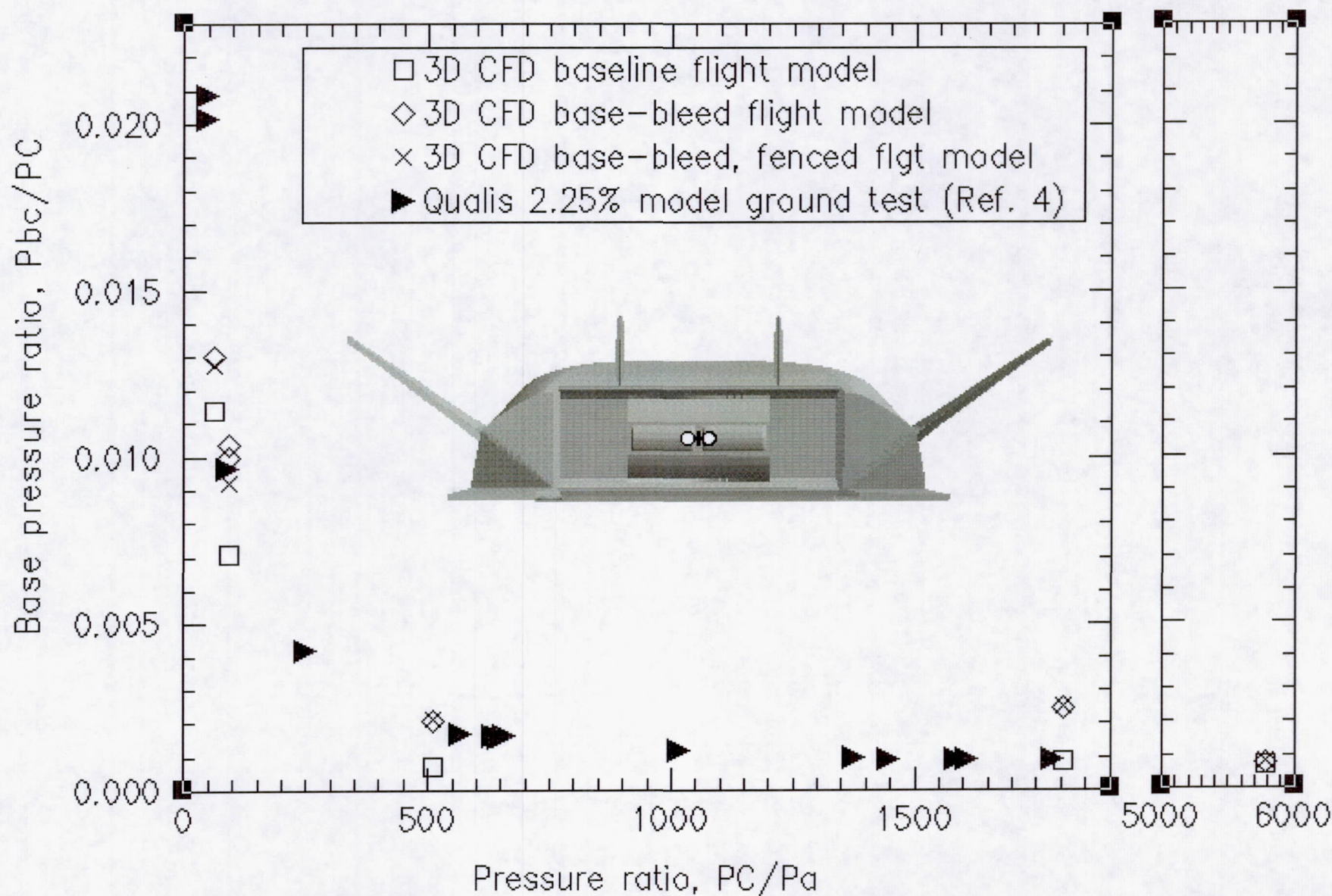
Comparison of Forebody and Aftbody Pressure Coefficients with a 7.75% Scaled Model Cold Flow Test



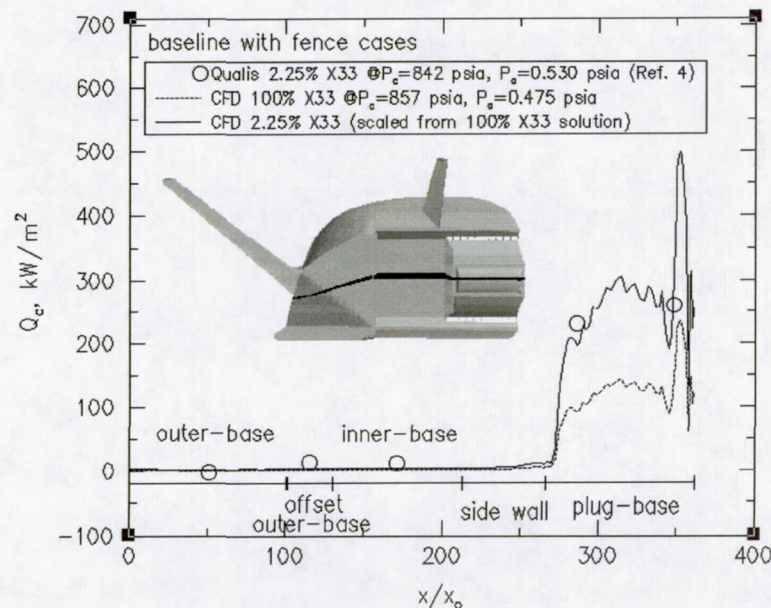
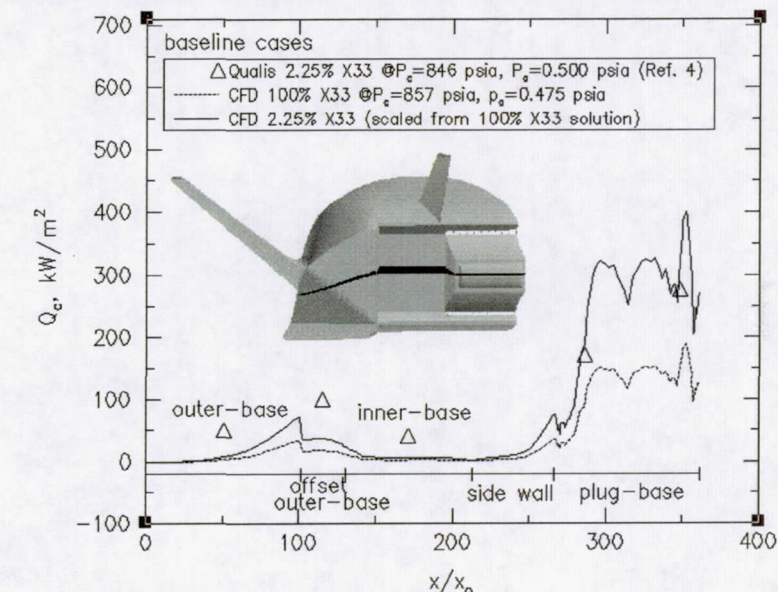
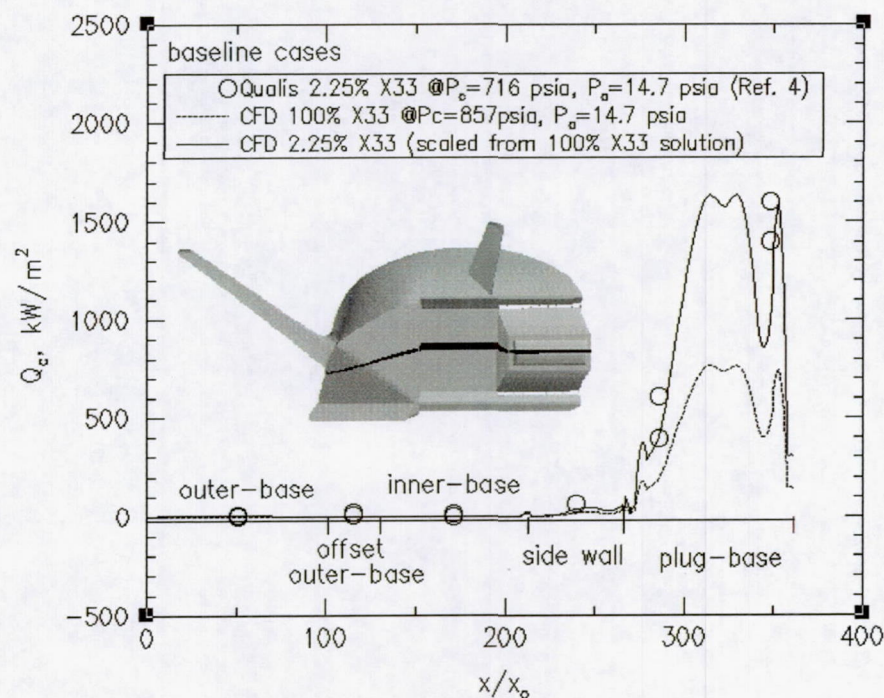
Comparison of Sea-Level Pillow Pressures with a 2.25% Scaled Model Hot-Fire Test



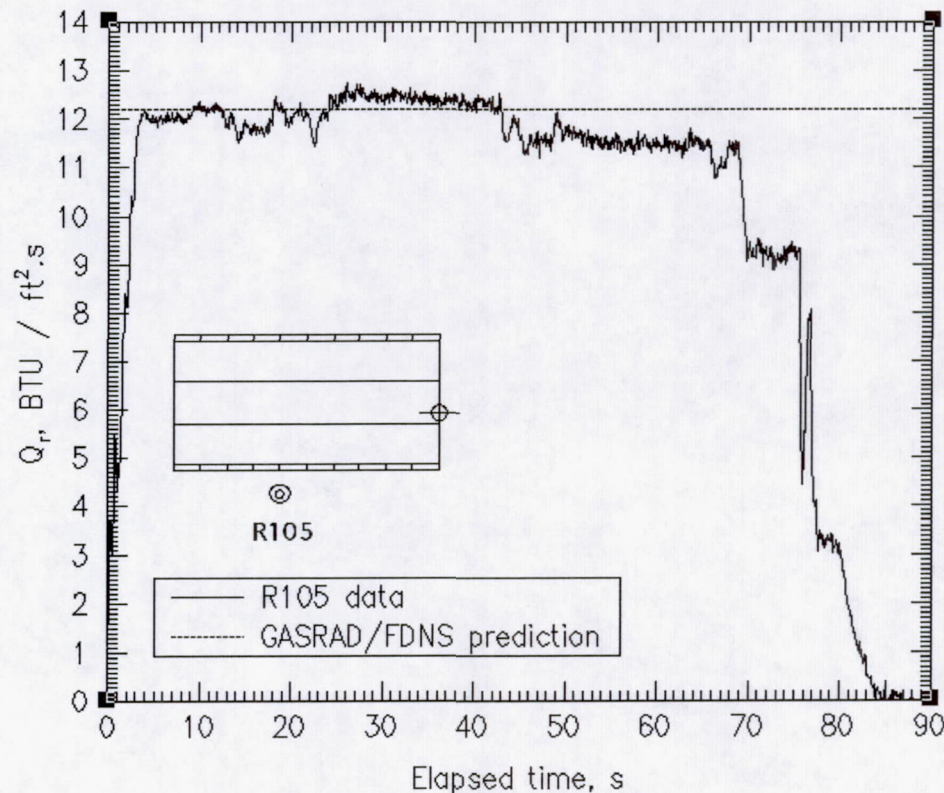
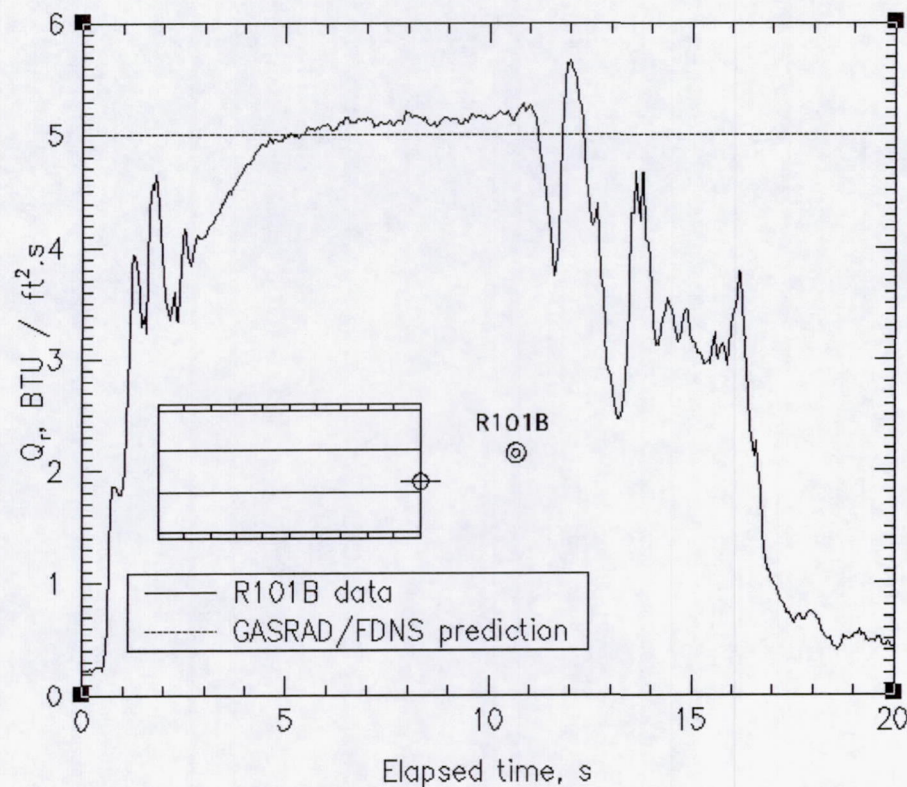
Comparison of Base Characteristic Pressures with a 2.25% Scaled Model Hot-Fire Test



Comparison of Base Horizontal Centerline Convective Heat Fluxes with a 2.25% Scaled Model Hot-Fire Test

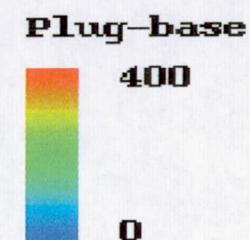
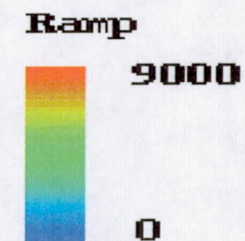
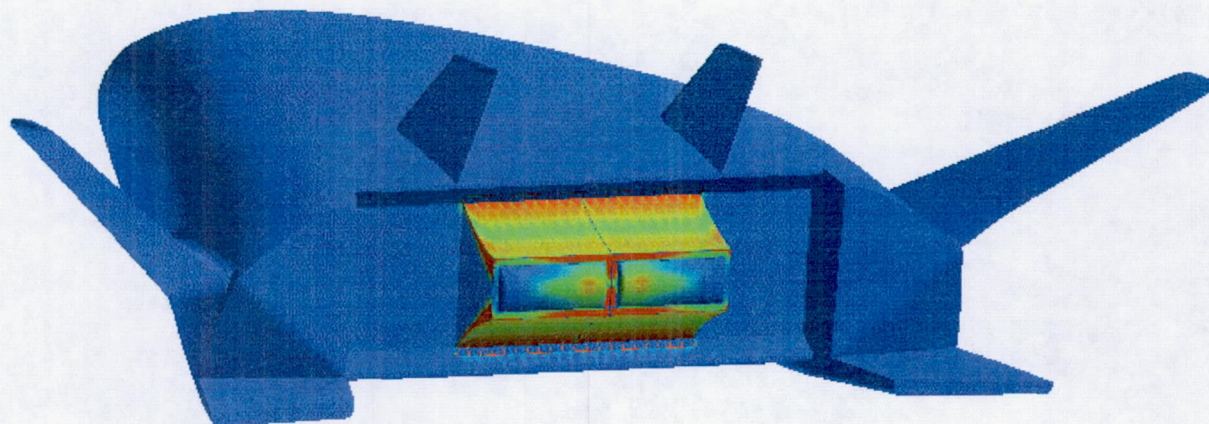


Comparison of Cowl and Inner-Base Radiative Heat Fluxes with an Installed Engine Test

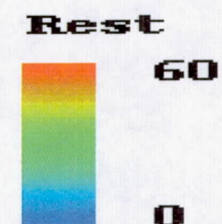
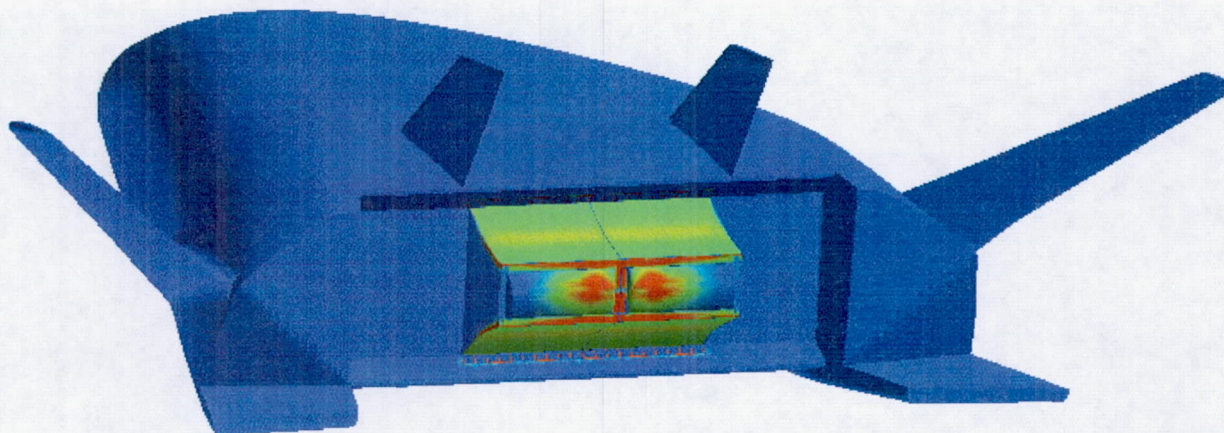


Preliminary Sea Level Q_c (KW/m²) Contours

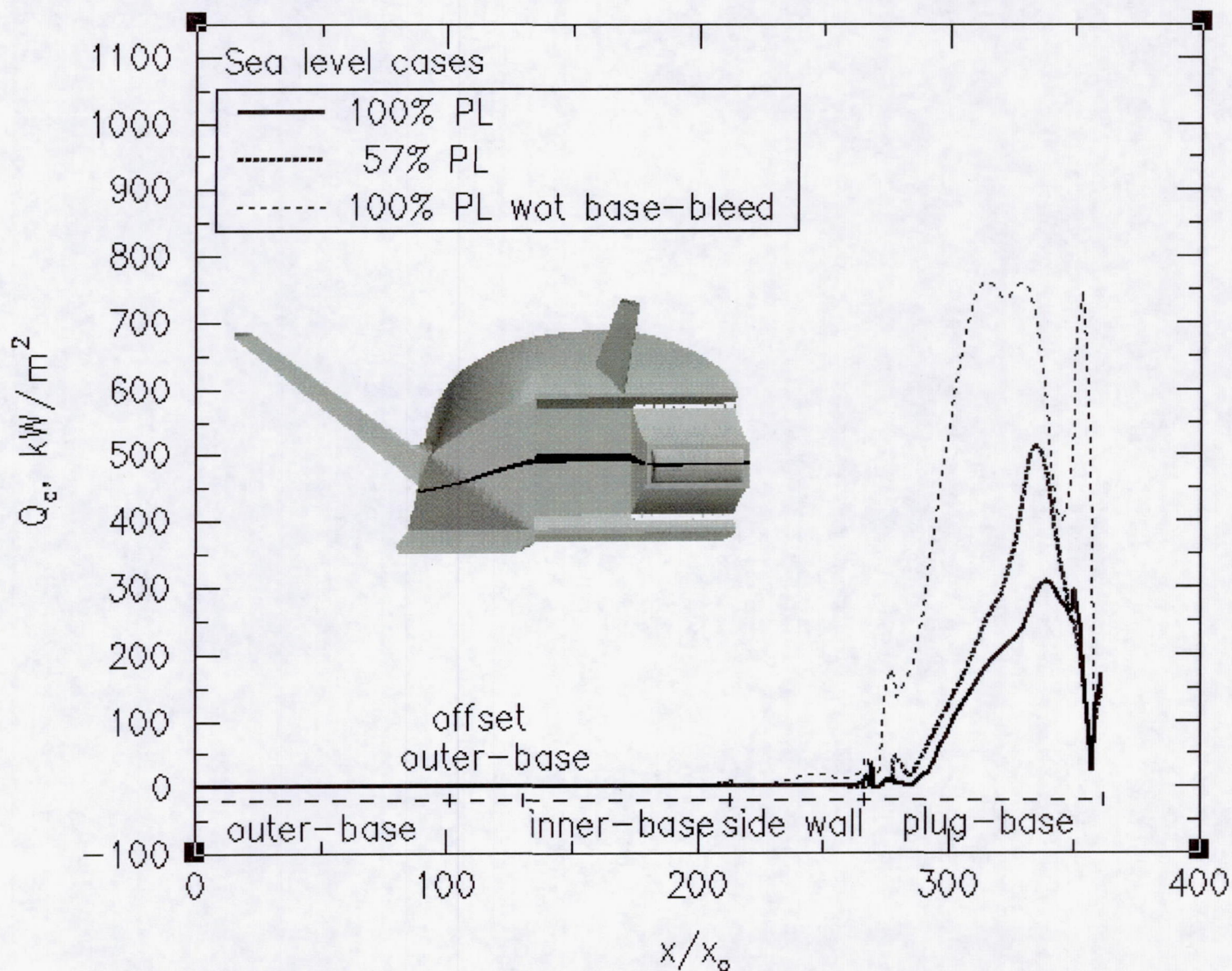
100% PL



57% PL



Preliminary Sea Level Q_c (KW/m²) Results





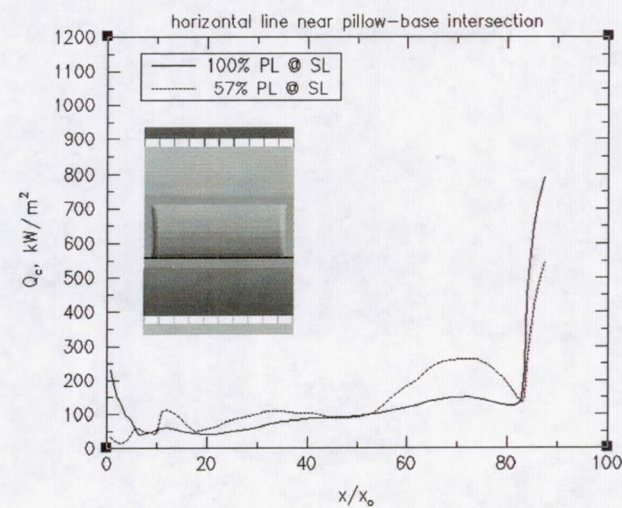
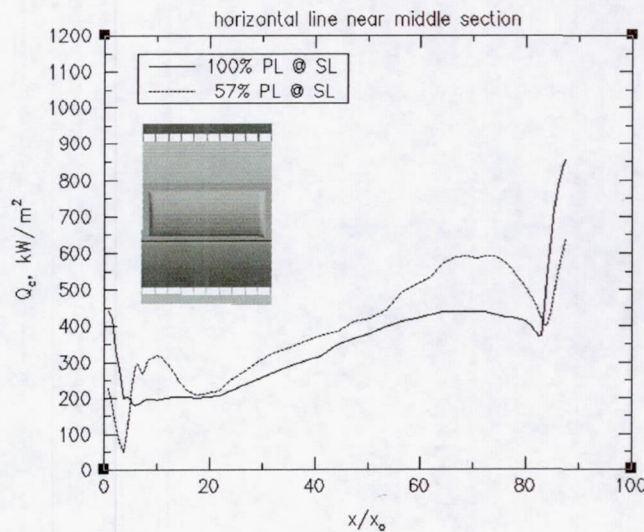
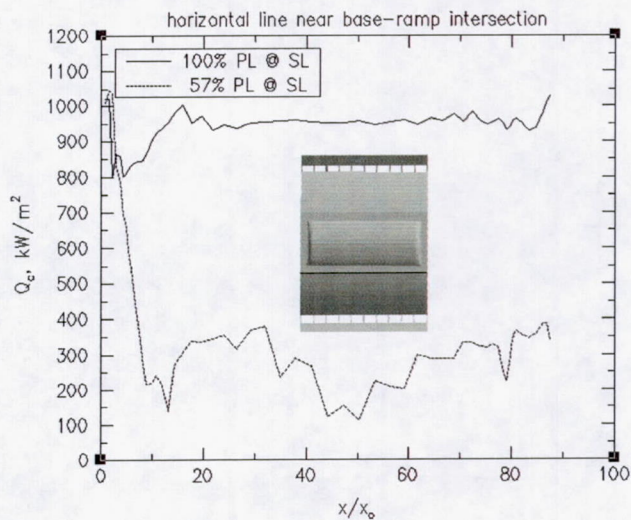
Preliminary Sea Level Q_c (KW/m²) Results



X-33 Lower Flex Seal Heat Fluxes

X-33 Lower Flex Seal Heat Fluxes

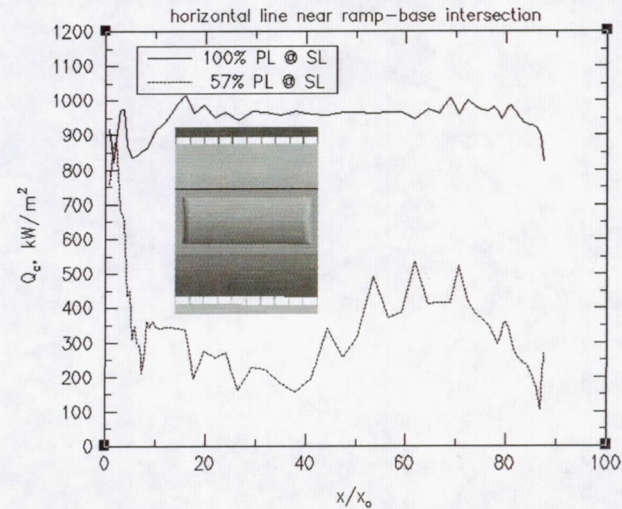
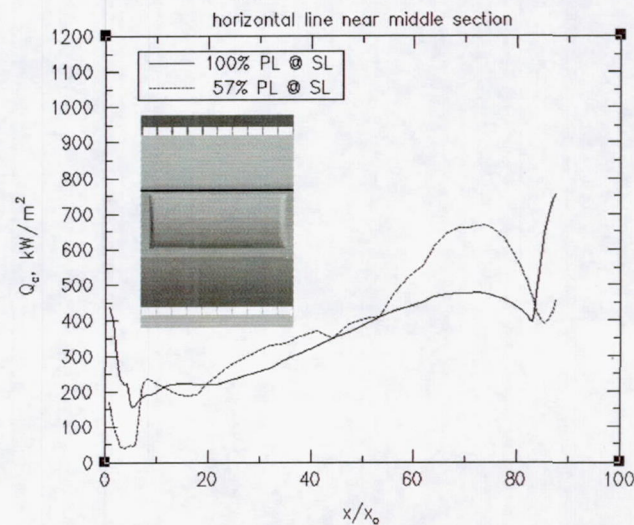
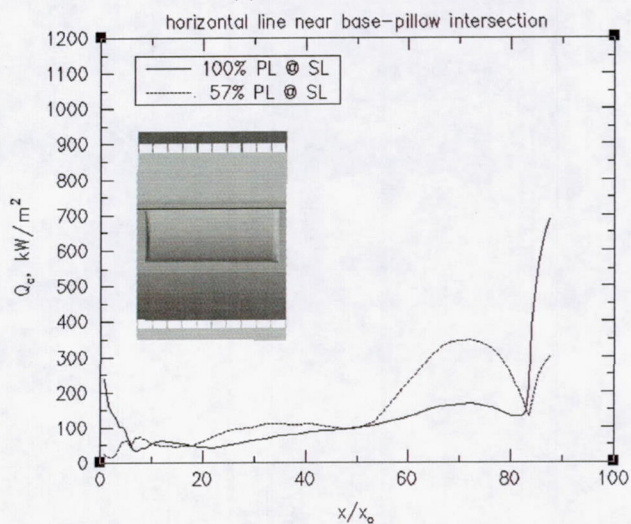
X-33 Lower Flex Seal Heat Fluxes



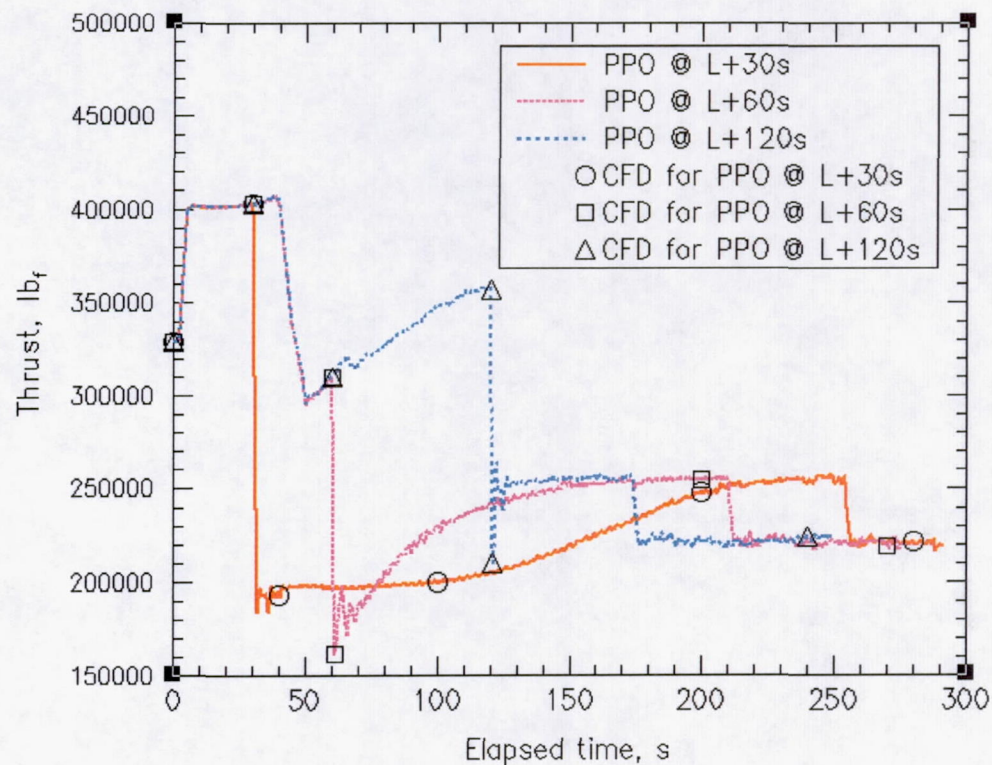
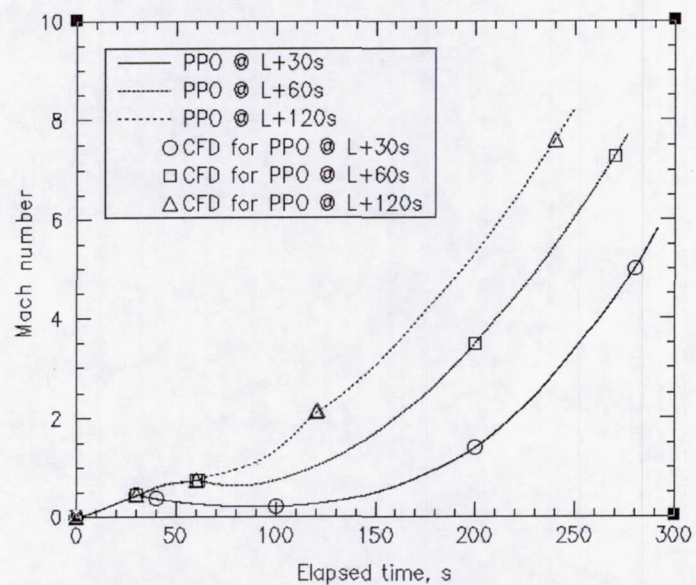
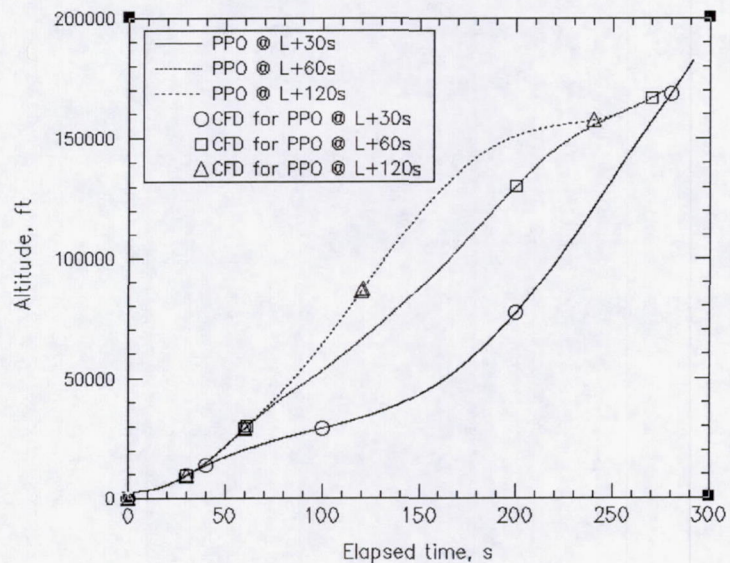
X-33 Upper Flex Seal Heat Fluxes

X-33 Upper Flex Seal Heat Fluxes

X-33 Upper Flex Seal Heat Fluxes



PPO Trajectory



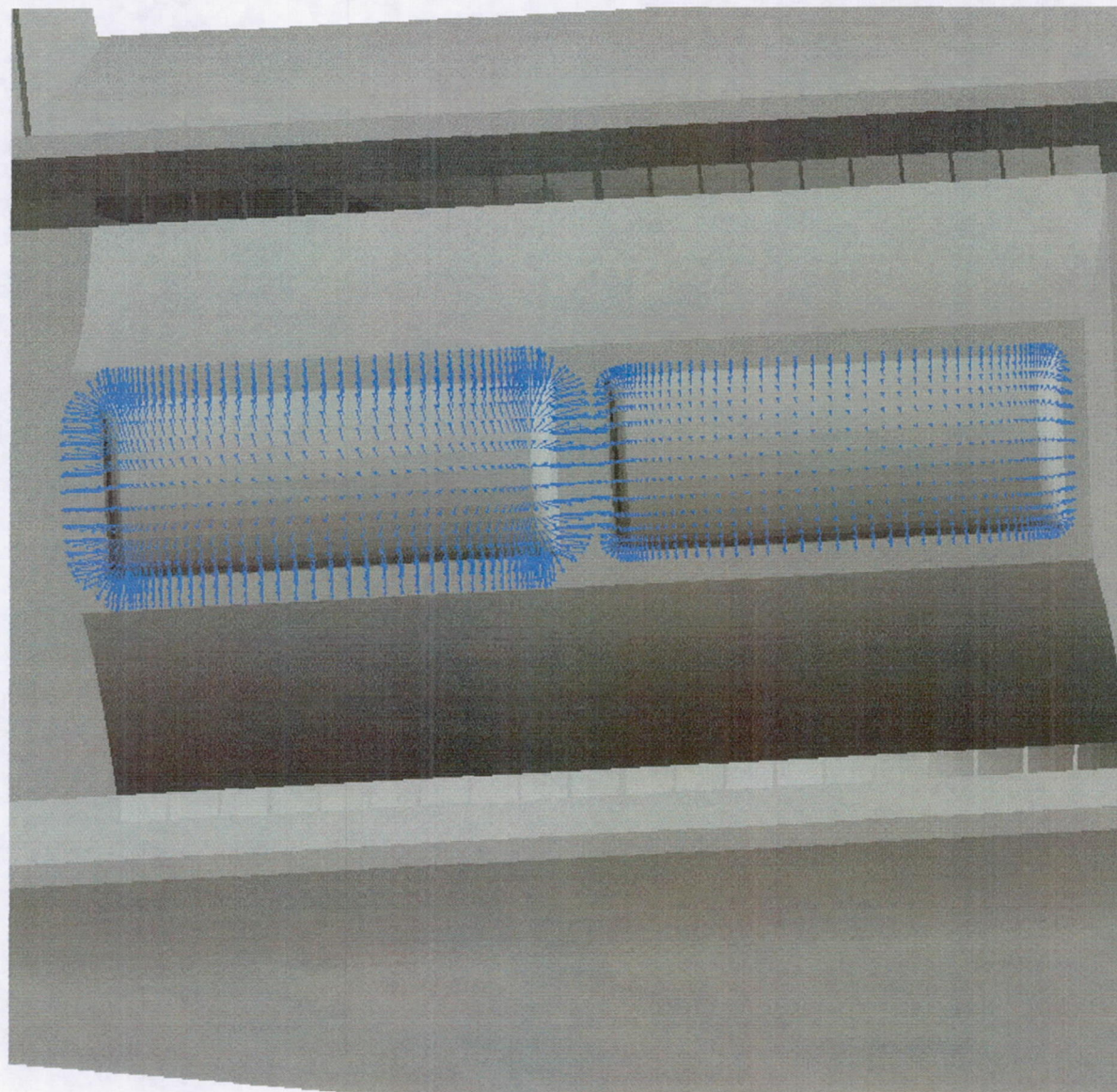


Run Matrix for PPO @ Launch + 30 s

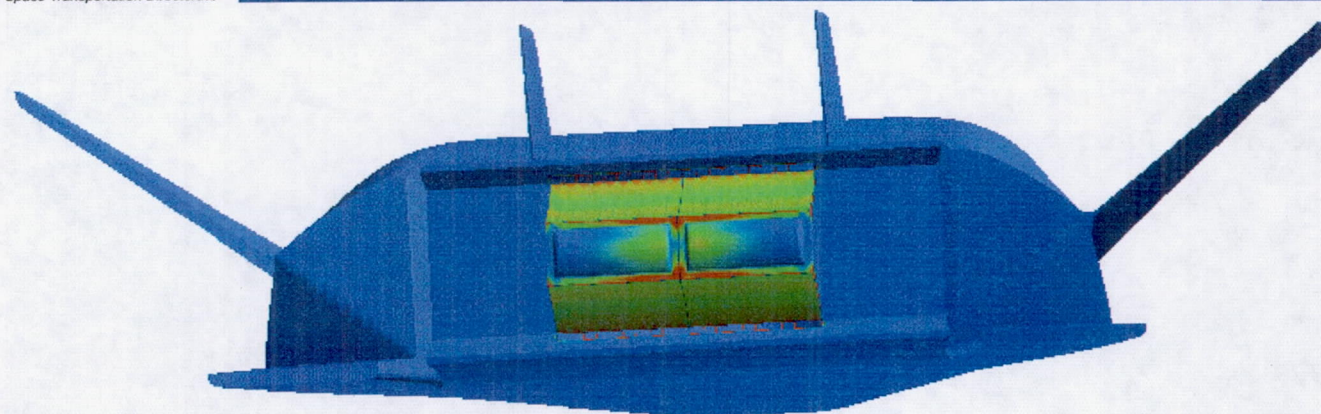


Case	t, s	M_{∞}	h, ft	$\%PL_{LE}$	$\%PL_{RE}$	$m_{LE,bb}$	$m_{RE,bb}$
1	0	0.00	0	82	80	9.9	9.7
2	30	0.44	9495	100	100	12.1	12.2
3	40	0.37	13821	49	48	9.0	2.9
4	100	0.21	28954	50	49	9.1	3.0
5	200	1.39	77217	51	48	9.1	3.0
6	280	5.00	168498	46	40	7.9	2.6

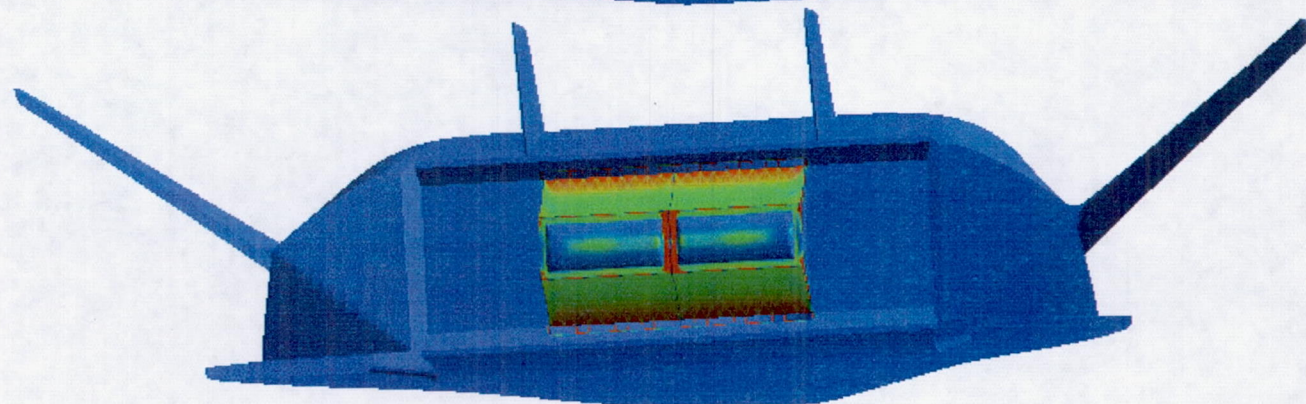
Base-bleed Vectors after a PPO



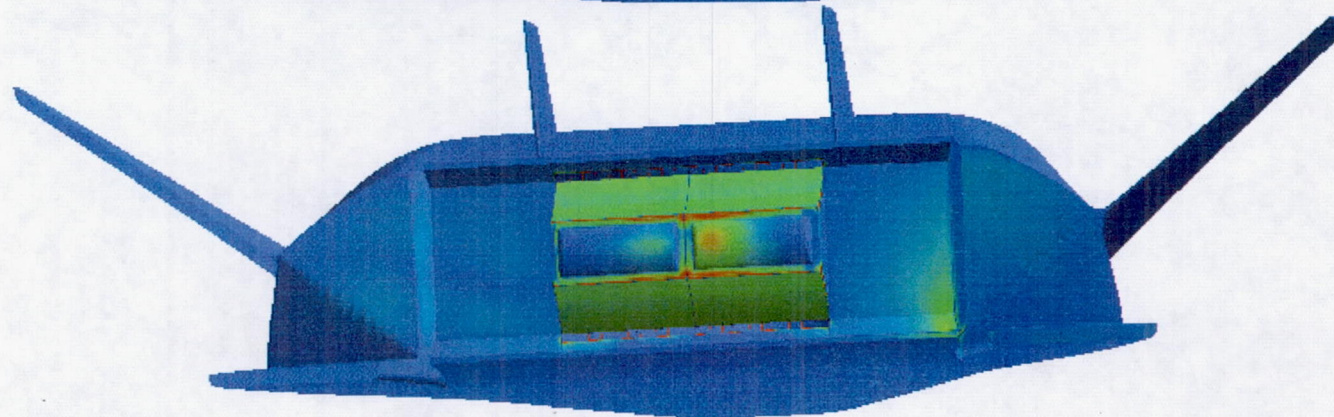
Preliminary Qc Contours for PPO @ Launch + 30 s



0 s

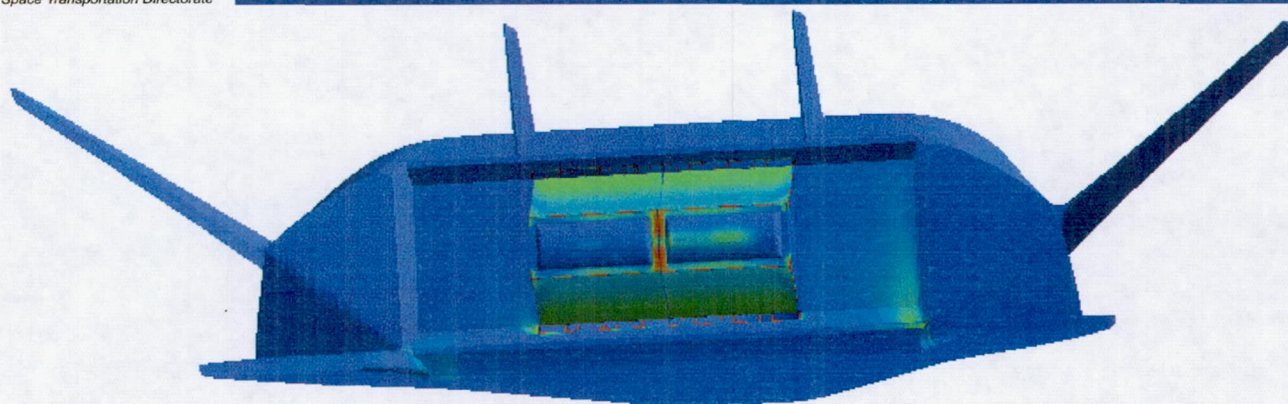


30 s

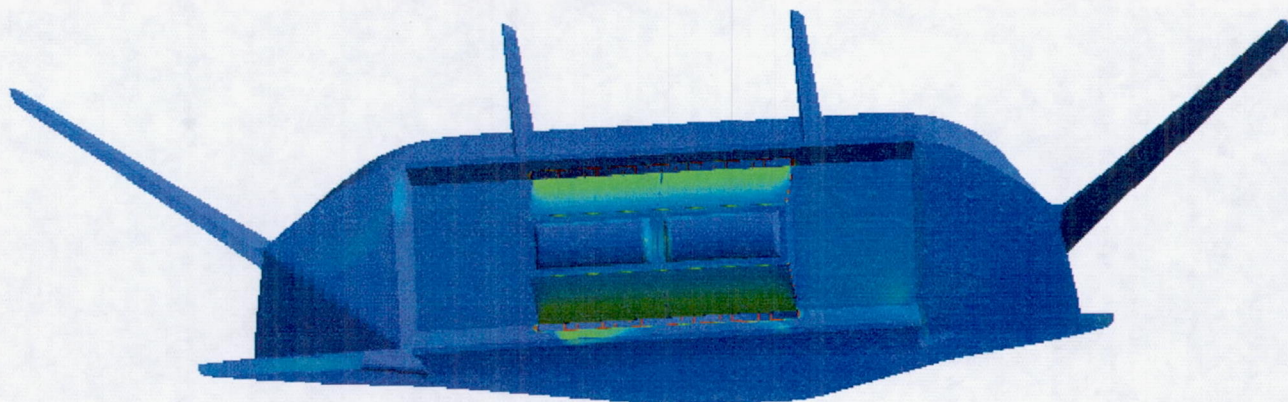


40 s

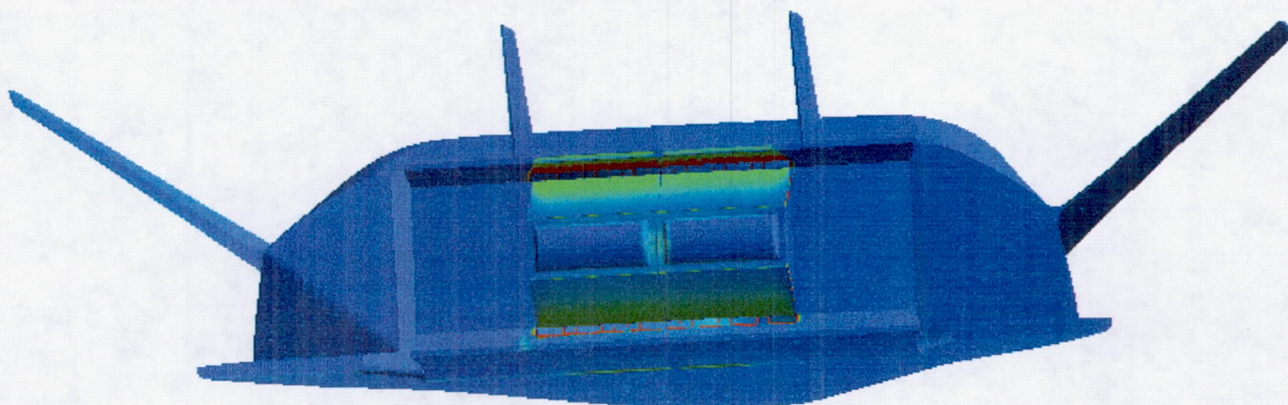
Preliminary Qc Contours for PPO @ Launch + 30 s



100 s



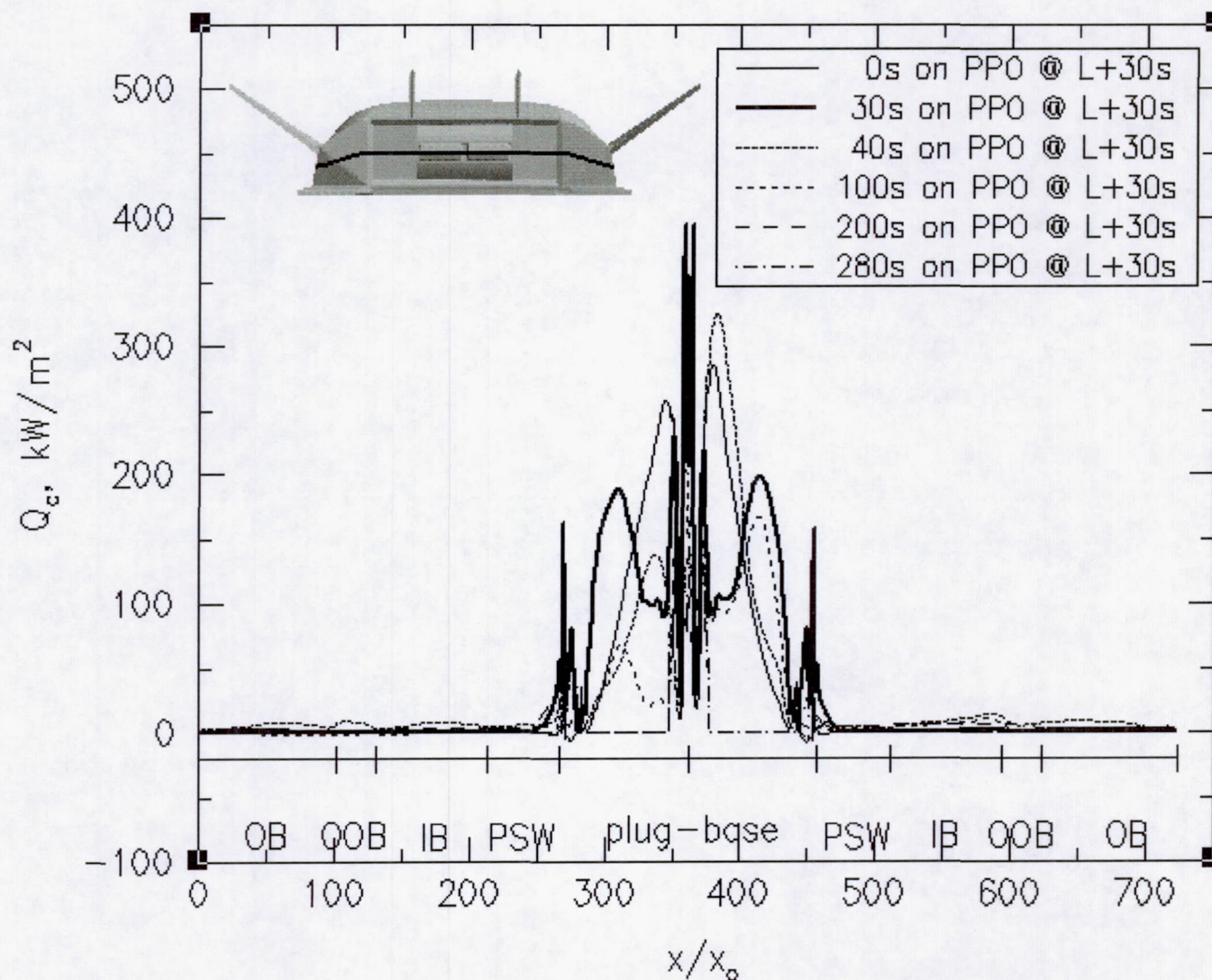
200 s



280 s

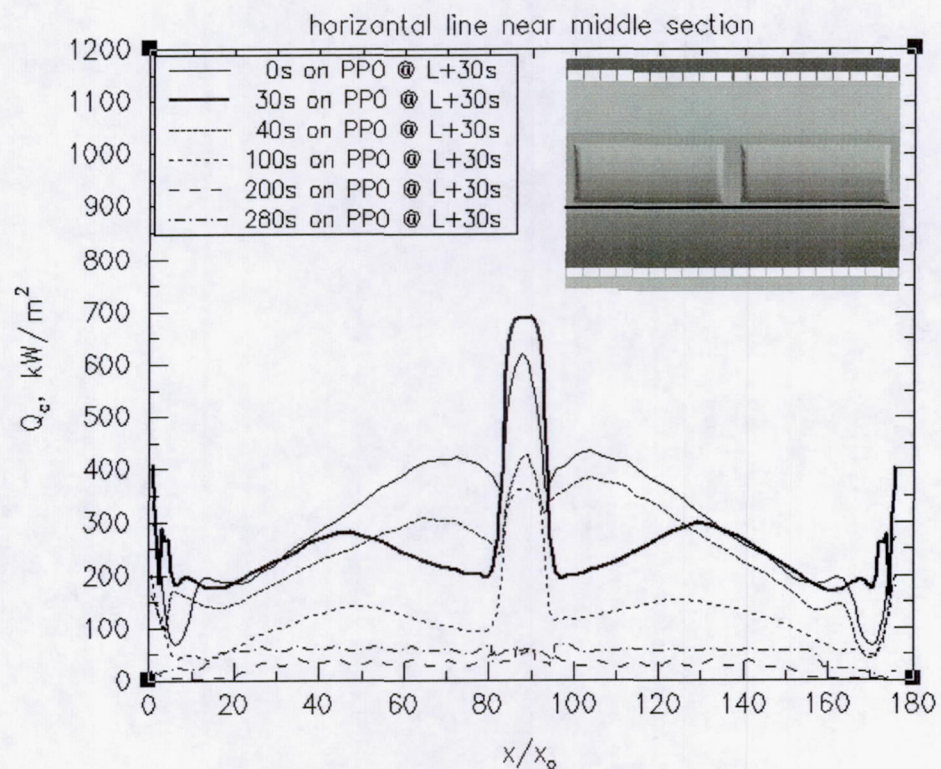
Preliminary Qc Results for PPO @ Launch + 30 s

base horizontal centerline

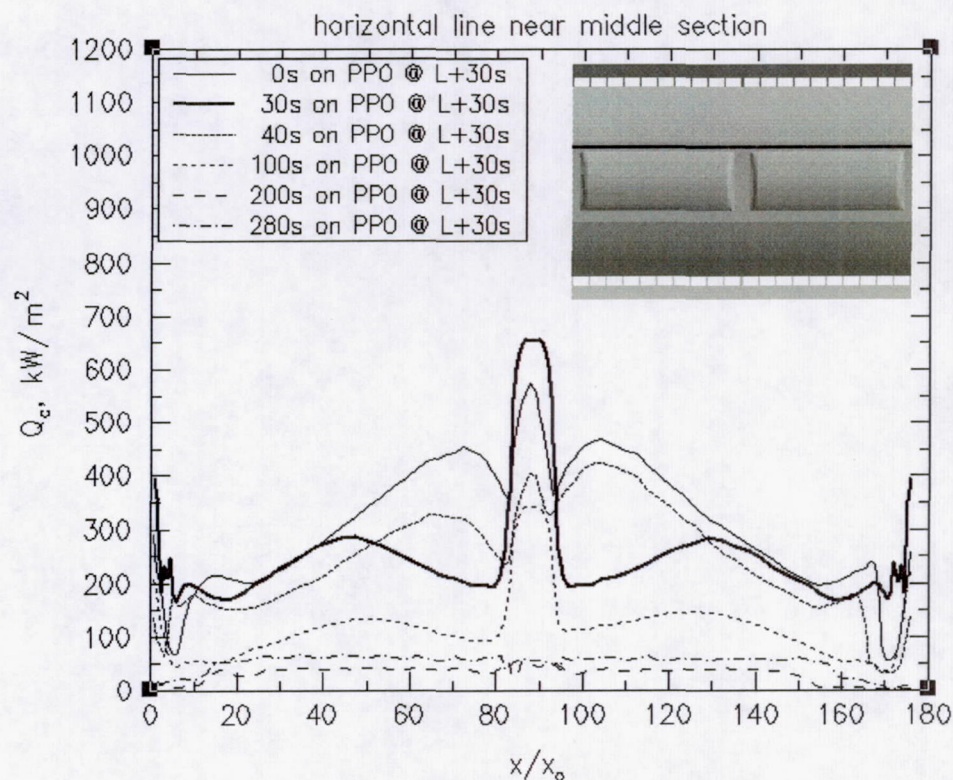


Preliminary Qc Results for PPO @ Launch + 30 s

X-33 Lower Flex Seal Heat Fluxes



X-33 Upper Flex Seal Heat Fluxes





Summary



- A systematically anchored computational fluid dynamics and heat transfer model is being used to study the effect of reduced power level on base-heating environment during sea level testing and during PPO.
- Preliminary results show that convective heating is higher for 57% PL than that for 100% PL on most of the pillows and flex seals during sea level testing. This agrees with test observations.
- Preliminary results of PPO @ L +30 s show that convective heating on pillows and flex seals on the “off” engine side is higher than that on the “on” engine side.
- Future work includes study of PPO @ L + 60 s and PPO @ L + 120 s trajectories to bracket the heating envelope and radiative heating calculations.